

Polymers in Solution

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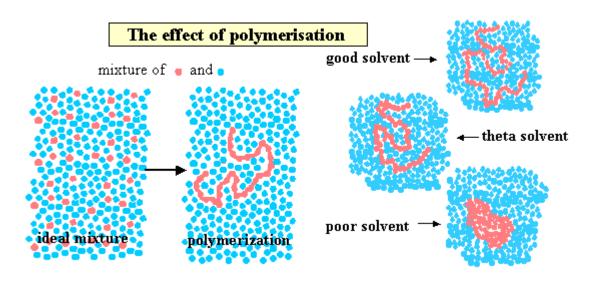




3. Thermodynamics of polymer solution and blends

1. Thermodynamic Classification of Solutions





Thermodynamic properties of the polymer solution depend on how "good" the solvent is for the polymer as well as on the polymer itself. The interaction between the solvent and the polymer and the degree of polymerization dictate the properties.

Second law of thermodynamics

$$\Delta G = \Delta H - \Delta(TS) = \Delta U + \Delta(pV) - \Delta(TS) = \Delta A + \Delta(pV)$$

 $G=Gibbs\ energy;\ H=enthalpy;\ U=internal\ energy;\ A=Helmholtz$ energy, free energy; $S=entropy,\ p=pressure,\ V=volume\ and\ T=thermodynamic\ temperature$

Mixing of two components: ideal + excess

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix}} = \Delta H_{\text{mix}} - T\Delta S_{\text{mix,id}} - T\Delta S_{\text{mix,ex}}$$

polymer coils

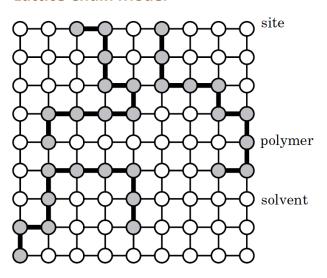
According to the various contributions, the solutions can be classified:

Type	ΔG_{mix}	ΔH_{mix}	$\Delta s_{ m mix,\ exc}$	Miscibility
Ideal	- TΔS _{mix,id}	0	0	At all T
Athermal	negative	0	positive	At all T
Regular	negative	negative	0	At all T
Irregular	negative	negative	positive	At all T
Pseudo-ideal (theta)	$- T\Delta S_{mix,id} \\ \sim 0$	$- \theta \Delta S_{mix,exc}$	$\Delta H_{mix}/\theta$	At θ

2. FLORY-HUGGINS MEAN-FIELD THEORY (1930)



Lattice Chain Model



The system consists of n_{site} sites. Each site can be occupied by either a monomer of the polymer or a solvent molecule. Polymer chains consisting of N monomers are laid onto empty sites one by one until there are a total nP chains. Then, the unoccupied sites are filled with solvent molecules.

	Volume Fraction	Number of Molecules		
Polymer Solvent	ϕ $1-\phi$	$n_{\rm P} = n_{\rm site} \phi / N$ $n_{\rm S} = n_{\rm site} (1 - \phi)$		

Entropy Mixing

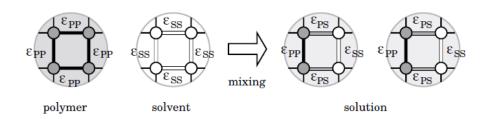
$$-\Delta S_{\text{mix}}/(k_{\text{B}} n_{\text{site}}) = \frac{\phi}{N} \ln \phi + (1 - \phi) \ln (1 - \phi)$$
 Flory-Huggins

 $\Delta S_{\rm mix}$ is greater than the entropy of mixing for an ideal solution. Greater number of conformations a polymer chain.

Flory's χ parameter or Flory-Huggins χ parameter-INTERACTION PARAMETER

Enthalpy of Mixing

$$\Delta G_{mix} = \Delta U_{mix} - T \Delta S_{mix}$$



$$\chi = \Delta U_{mix} / (kT N_s \phi_p)$$

Interaction Change Upon Mixing

$$\Delta U_{\text{mix}}/(n_{\text{site}}k_{\text{B}}T) = \chi\phi(1-\phi)$$
 Flory-Huggins

 ΔU_{mix} depends on the interaction through $\chi.$ A system with the same χ has the same ΔU_{mix}

A solution with $\chi = 0$ is called **an athermal solution.**

3. Free Energy, Chemical Potentials, and Osmotic Pressure



Helmholtz free energy of mixing

$$\Delta A_{\text{mix}} = \Delta U_{\text{mix}} - T \Delta S_{\text{mix}}$$

$$\frac{\Delta A_{\text{mix}}}{n_{\text{site}}k_{\text{B}}T} = \frac{\phi}{N}\ln\phi + (1-\phi)\ln(1-\phi) + \chi\phi(1-\phi)$$
 Flory-Huggins

Chemical Potentials

$$\frac{\Delta \mu_{\rm S}}{k_{\rm B}T} = \left(\frac{\partial}{\partial n_{\rm S}} \frac{\Delta G_{\rm mix}}{k_{\rm B}T}\right)_{T,p,n\rm P} = \ln(1-\phi) + \left(1-\frac{1}{N}\right)\phi + \chi\phi^2$$

Osmotic Pressure

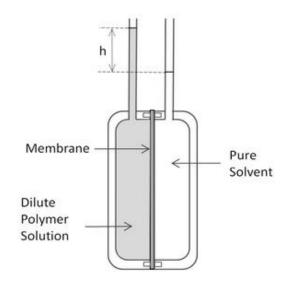
$$\frac{\varPi v_{\text{site}}}{k_{\text{B}}T} = \frac{\varPi V}{n_{\text{site}}k_{\text{B}}T} = \frac{\phi}{N} - \ln(1 - \phi) - \phi - \chi \phi^2 \qquad \text{Flory-Huggins}$$

3. Free Energy, Chemical Potentials, and Osmotic Pressure



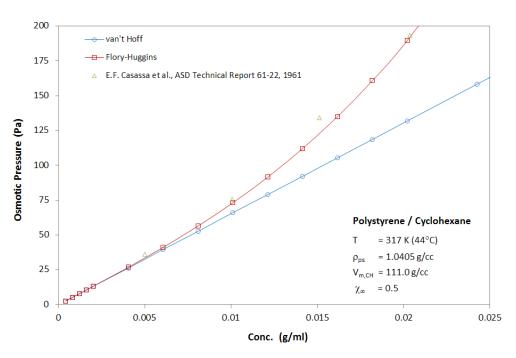
Osmotic Pressure of Polymer Systems

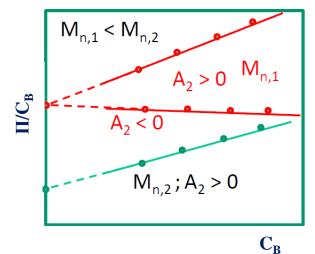
SIMPLE MEMBRANE OSMOMETER



$$\frac{\pi}{c_B} = RT \left(\frac{1}{M_n} + A_2 c_B \right)$$

Determination of M_n and A₂





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2. FLORY-HUGGINS MEAN-FIELD THEORY (1930)



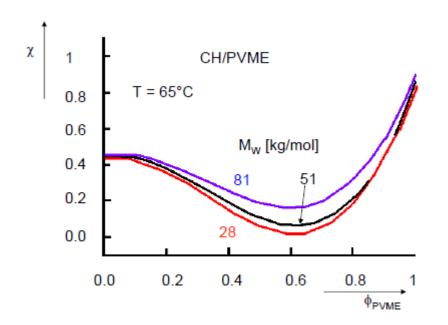
$$\chi(T) = A + B / T$$

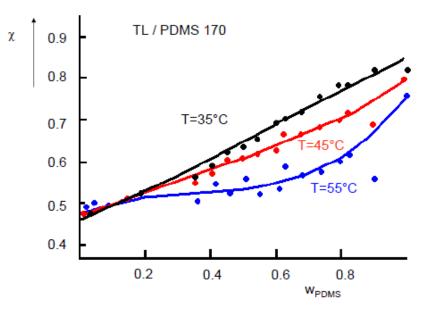
The temperature independent term A is the so-called "entropic part" of of χ , while B / T is called the "enthalpic part".

The parameter *A* and *B* have been tabulated for many polymer-solvent and polymer-polymer systems.

Flory-Huggins parameter for polymer + solvent - systems

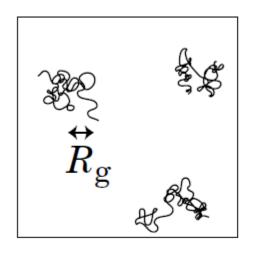
system	T [°C]	χ	
cellulose nitrate + acetone	25	0.27	
polyisobutylene + benzene	25	0.5	
polystyrene + toluene	25	0.44	
PVC + THF	26	0.15	
rubber + CCl ₄	20	0.28	
rubber + benzene	25	0.44	
rubber + acetone	25	1.37	

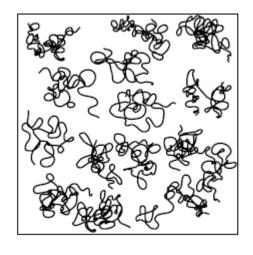


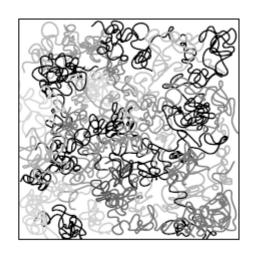




Concentration Regimes for Linear Flexible Polymers







$$c \ll c^*$$

$$c\cong c^*$$



Dilute

The polymer chain interacts primarily with the solvent molecules. The solution is close to an ideal solution.

Semidilute

The thermodynamic properties of the semidilute solutions are greatly different from those of an ideal solution extrapolated to the same concentration.

The existence of the semidilute regime is characteristic

of the polymer solutions.

$$c_*[\eta] = 1$$

Chains are overlapped and entangled. Their mobility is greatly reduced compared with the chains in dilute solutions.



Concentration Regimes for Linear Flexible Polymers

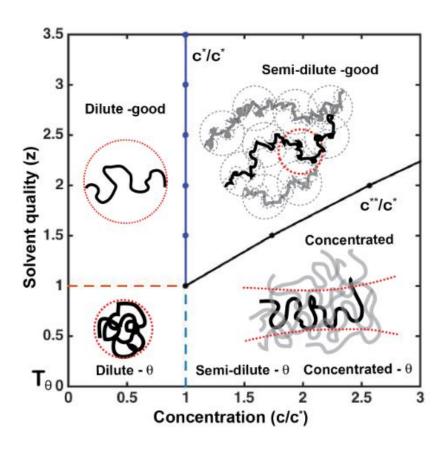
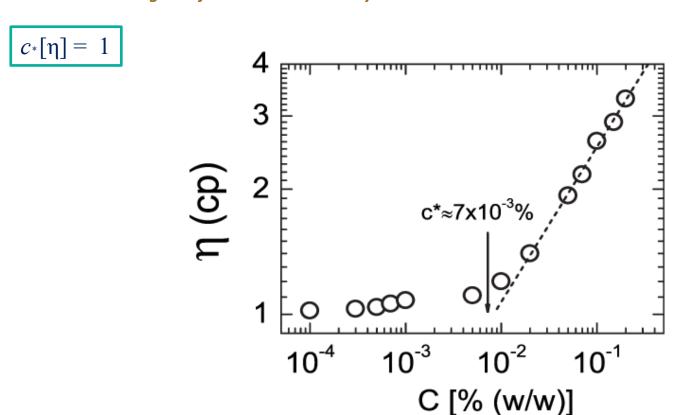


FIG. 1. Phase diagram for polymer solutions as a function of relative concentration c/c^* and solvent quality z (see Section II for details). For display purposes, we chose monomer size b=1 and an excluded volume exponent $\nu=0.56$ based on experimental results.



Concentration Regimes for Linear Flexible Polymers

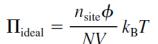


The critical polymer concentration c * is determined as the concentration at the onset of the power law behavior of the viscosity as a function of polymer concentration c.



Osmotic compressibility (Π/Π_{ideal})

$$\frac{\Pi V}{n_{\text{site}}k_{\text{B}}T} = \frac{\phi}{N} + \left(\frac{1}{2} - \chi\right)\phi^2 + \frac{1}{3}\phi^3 + \cdots$$
 Flory-Huggins, dilute solution



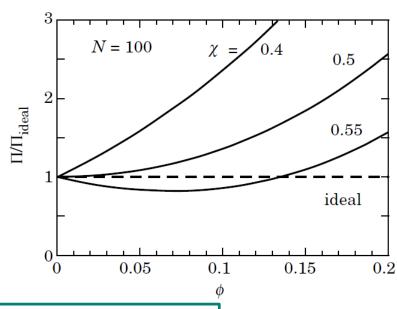


Figure 2.7. Osmotic compressibility (Π/Π_{ideal}) plotted as a function of ϕ for the ideal solution (dashed line) and nonideal solutions with N=100 and $\chi=0.4, 0.5$, and 0.55 (solid lines).



Virial Expansion

$$\frac{\Pi}{N_{\rm A}k_{\rm B}T} = \frac{c}{M} + A_2c^2 + A_3c^3 + \cdots \quad \text{virial expansion}$$

$$c = \frac{M}{N_{\rm A}N} \frac{\phi}{v_{\rm site}}$$

$$A_2 = \left(\frac{1}{2} - \chi\right) N_{\rm A} v_{\rm site} (N/M)^2$$

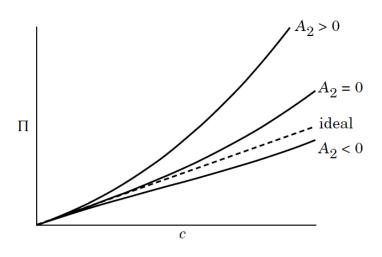
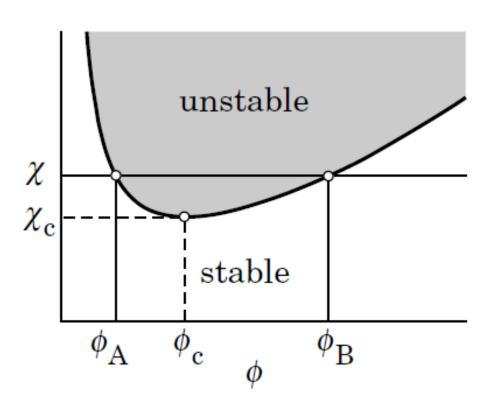


TABLE 2.4 Relationship Between A_2 and χ

A_2	П	χ
+ 0 -	$>\Pi_{ ext{ideal}}$ $\cong \Pi_{ ext{ideal}}$ $<\Pi_{ ext{ideal}}$	<1/2 =1/2 >1/2



Coexistence Curve and Stability



The instability condition is given as

$$\frac{1}{\phi} + \frac{N}{1 - \phi} < 2\chi N$$

The line that separates the stable region from the unstable region is called the **spinodal line**.



PHASE DIAGRAM AND THETA SOLUTIONS

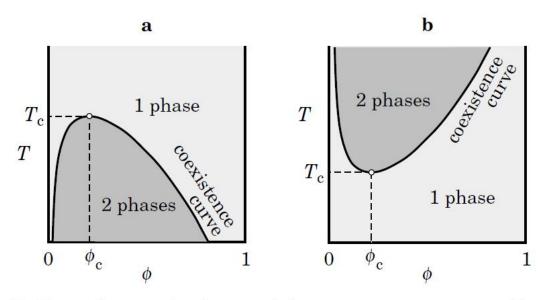


Figure 2.19. Phase diagram of polymer solution on temperature—composition plane. a: UCST-type phase diagram. b: LCST-type phase diagram. The critical point is at the apex of the coexistence curve and is specified by the critical temperature T_c and the critical composition ϕ_c .

The temperature at the critical condition is called the **critical temperature**.

The phase diagram has the critical temperature (Tc) at the highest point on the coexistence curve- **upper critical solution** temperature (UCST).

The phase diagram has the critical temperature (Tc) at the lowest point on the coexistence curve-lower critical solution temperature (LCST).



PHASE DIAGRAM AND THETA SOLUTIONS

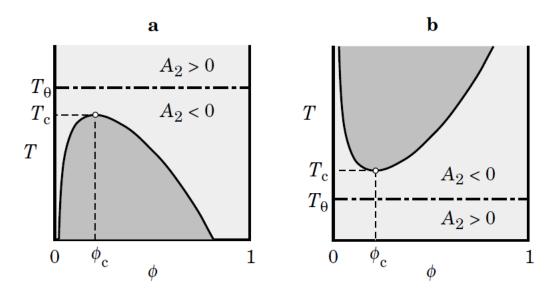


Figure 2.23. Relationship between the theta temperature T_{θ} with the critical temperature T_{c} . a: UCST-type phase diagram. b: LCST-type phase diagram. The second virial coefficient A_{2} changes its sign at $T = T_{\theta}$.

The Theta-temperature $(A_2 = 0)$ is the temperature for the particular theta-solvent which minimizes interactions between the polymer segments and the solvent. The theta temperature is different for each combination of polymer and solvent.

There is a slight molecular weight dependence of the temperature that renders $A_2 = 0$ when the molecular weight is not sufficiently high. The dependence is much smaller compared with the dependence of Tc on the molecular weight.



Solubility Parameter

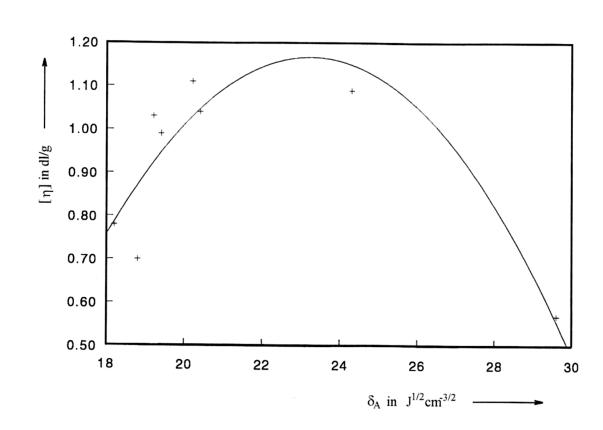
$$\chi = \frac{V_{\rm S}}{N_{\rm A}k_{\rm B}T}(\delta_{\rm S} - \delta_{\rm P})^2 + 0.34$$

$$\Delta H_m = n v_A \varphi_B (\delta_A - \delta_B)^2$$

$$\delta = \sqrt{\frac{\Delta H_v - RT}{V}}$$

Experimental determination of δ :

At $\Delta H_m = 0$, $\delta_A = \delta_B$ having maximum intrinsic viscosity [η], which means maximum coil expansion





Solubility Parameter

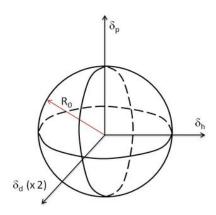
Hansen's Three-dimensional solubility Parameter

$$\delta^2 = \delta_d^2_{(dispersion forces)} + \delta_p^2_{(polar forces)} + \delta_H^2_{(hydrogen bonding)}$$

The method is based on the idea that *like dissolves like*. This is the case when the solvent and the solute have similar Hansen Solubility Parameters.

Polymer/Solvent	Hansen Parameters ^a		Solubility	
	δ_D	δ_P	δ_H	Δ_{total}
Polyacrylonitrile (PAN)	21.7	14.1	9.1	27.4
N,N-Dimethyl formamide (DMF)	17.4	13.7	11.3	24.9
Dimethyl Acetamide (DMAc)	16.8	11.5	10.2	22.7
Toluene	18.0	1.4	2.0	18.2
Ethanol	15.8	8.8	19.4	26.5 2
Ethylene glycol (EG)	17.0	11.0	26.0	32.9
Distilled water	16.6	16.0	42.3	48.2

HANSEN SOLUBILITY SPHERE



$$R_a^2 = 4(\delta_{d2} - \delta_{d1})^2 + (\delta_{p2} - \delta_{p1})^2 + (\delta_{h2} - \delta_{h1})^2$$

The distance R_a in the equation above can be compared with the solubility radius of the polymer, R_0 .

The radius of the solubility sphere is often called the interaction radius and the ratio $R_{\rm a}$ / $R_{\rm 0}$ the relative energy difference (RED) of the system.

 $R_{\rm a}/R_0 > 1$ \rightarrow the compound is a non-solvent $R_{\rm a}/R_0 < 1$ \rightarrow the compound is a solvent $R_{\rm a}/R_0 = 0$ \rightarrow the compound may cause swelling



If **two polymers are mixed**, the most frequent result is a system that exhibits **a complete phase separation due to the repulsive interaction between the components**. Complete miscibility in a mixture of two polymers requires that the following condition is fulfilled:

$$\Delta G_{\rm m} = \Delta H_{\rm m} - T\Delta S_{\rm m} < 0$$

a) The value of $T\Delta S_m$ is always positive \rightarrow there is an increase in the entropy on mixing.

$$\Delta G_{\rm m} < 0, \left(\frac{\partial^2 \Delta Gm}{\partial \phi^2}\right)_{\rm p,T} > 0$$

b) The sign of ΔG_m always depends on the value of the enthalpy of mixing $\Delta H_m \Delta H_m < T\Delta S_m$

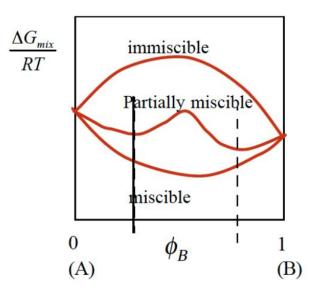
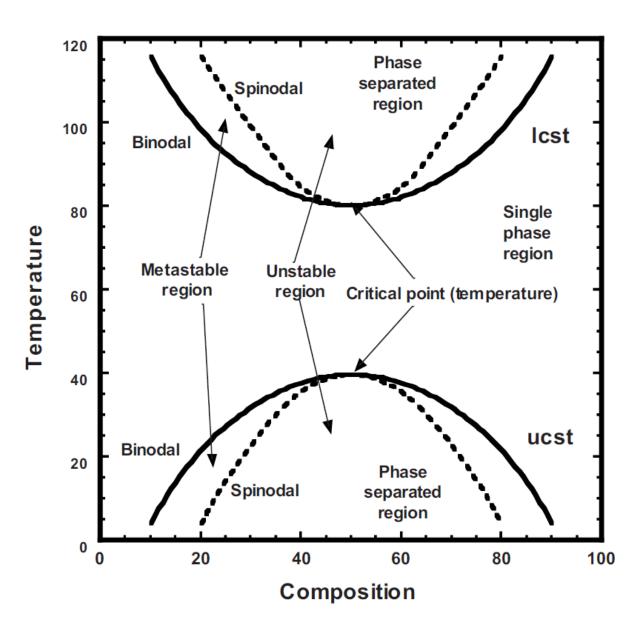


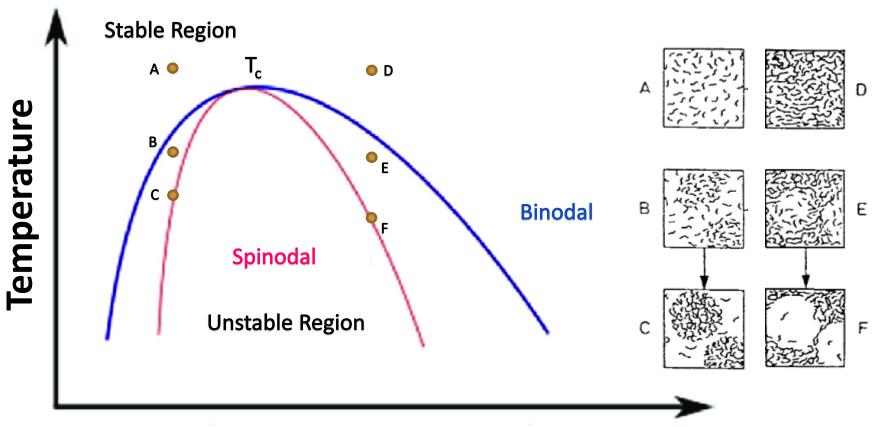
Figure 2. Gibbs free energy for miscible and immiscible polymer combinations



$$\left(\frac{\partial^2 \Delta Gm}{\partial \phi^2}\right)_{p,T} = 0 \quad Spinodal$$







Polymer concentration

Binodal: Nucleation and growth separation in small spherical regions of the 2nd phase, which grow over time.

Spinodal: Phase separation as small overlapping worm structures (interconnected phase domains). After spinodal decomposition, coarsening of the structures in spheroidal domains.



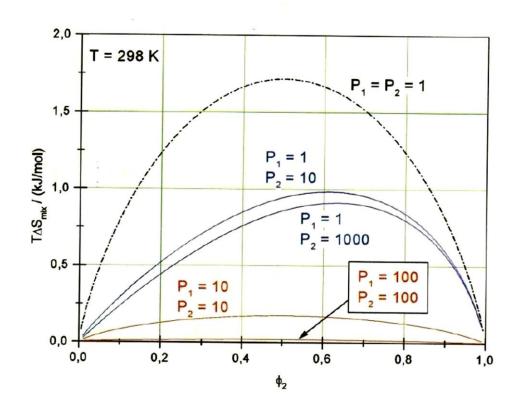
Entropy of mixing for polymer blends

$$\Delta S_{\rm m} = -R \left[\frac{\varphi_1}{r_1} \ln \varphi_1 + \frac{\varphi_2}{r_2} \ln \varphi_2 \right]$$

A large entropy of mixing for small molecule solutions!

Enormous differences in the entropy of mixing for polymer solutions versus regular solutions versus polymer blends!

 ΔS_m , polymer-polymer $< \Delta S_m$, polymer-small molecule $< \Delta S_m$, small molecules





Enthalpy of Mixing

$$\Delta G_{\rm m} = RT \left[\frac{\varphi_1}{r_1} \ln \varphi_1 + \frac{\varphi_2}{r_2} \ln \varphi_2 + \chi \Phi_1 \Phi_2 \right]$$

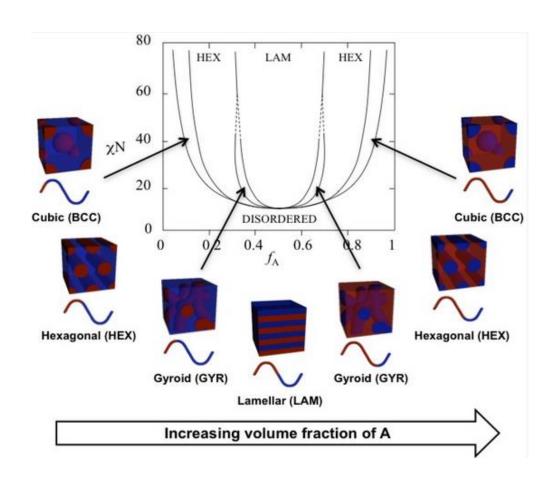
$$\Delta H_{\rm m} = RT \chi \Phi_1 \Phi_2$$

$$\chi_{\rm cr} = 1/2 \left[\frac{1}{\sqrt{r_1}} + \frac{1}{\sqrt{r_2}} \right]$$

- Most pairs of high molar mass polymers are immiscible. The positive mixing enthalpy together with negligible entropy contribute to the free energy of mixing.
- The enthalpy of mixing is primarily dependent on the energy change associated with changes during mixing. It is much less dependent on chain lengths. In the enthalpy of polymers mixing $\Delta H < 0$, the interaction energy between heterogeneous molecules is higher than between homogeneous ones. **Enthalpy contributions often dominate the free energy of mixing in polymeric systems.**
- The introduction of interacting groups by chemical modification of a polymer or by copolymerization leads to negative contributions to the enthalpy of mixing. This has been shown to lead to improved miscibility of an otherwise incompatible polymer pair.

4. Microphase Separation in block copolymers





The **particular structure** adopted by a block copolymer depends on the following **controllable parameters**;

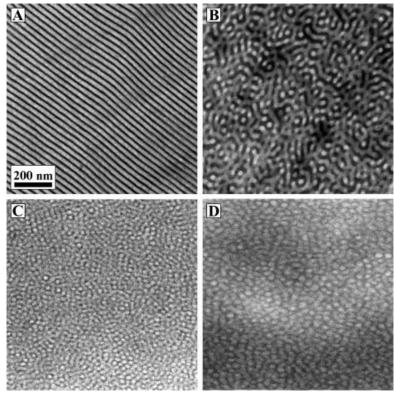
- (i) the Flory-Huggins interaction parameter χ
- (ii) the overall **degree of polymerisation N**
- (iii) the **volume fraction** of the component blocks, f,
- (iv) the particular **polymer architecture**

$$\chi = \frac{A}{T} + B$$

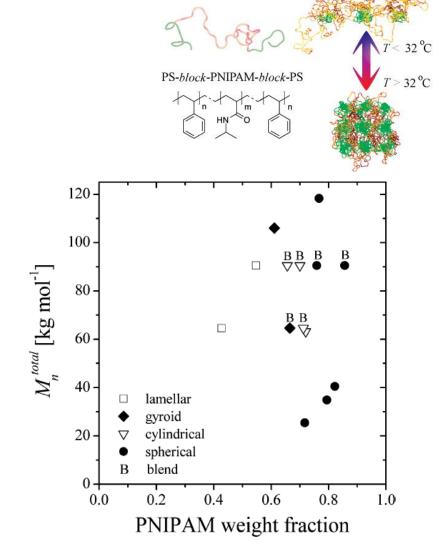
4. Microphase Separation in block copolymers. Examples



Phase Behavior and Temperature-Responsive Molecular Filters Based on Self-Assembly of Polystyrene-*block*-poly(*N*-isopropylacrylamide)-*block*-polystyrene



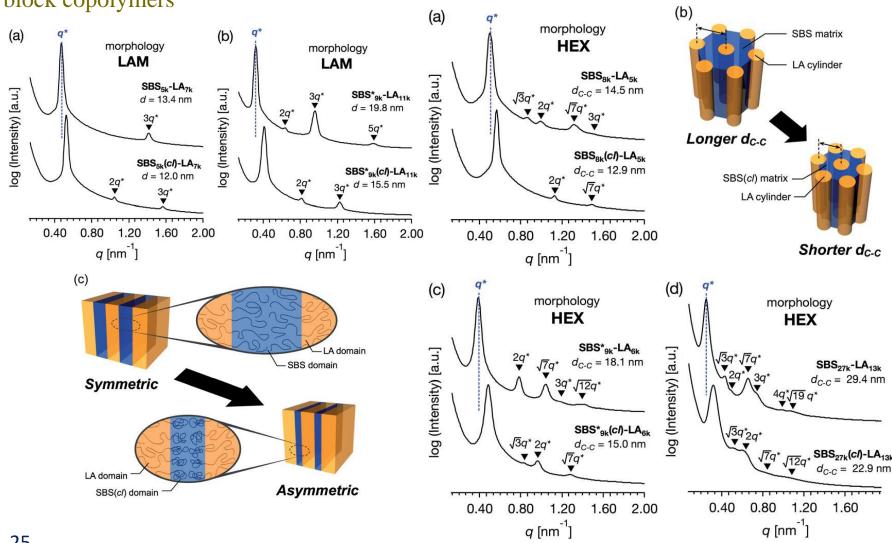
Representative TEM micrographs of pure PS-b-PNIPAMb-PS triblock copolymers in bulk: (A) PN43.65K (43 wt % PNIPAM) is **lamellar**, (B) PN61.106K (61 wt % PNIPAM) is **gyroid**, (C) PN72.63K (72 wt % PNIPAM) is **cylindrical/wormlike**, and (D)PN77.118K is **spherical**.



4. Microphase Separation in block copolymers. Examples



Downsizing feature of microphase-separated structures via intramolecular crosslinking of block copolymers



Example questions



- (1) How can you determine the overlap concentration c* experimentally? Why should experiments be performed in dilute solutions in order to obtain molecular parameter?
- (2) Define theta-temperature
- (3) How can you experimentally determine HUGGINS-interaction parameter χ ?
- (4) What can you say about the solubility of a polymer and its conformation if you know that it is monodisperse with $\chi > 0.5$ in the corresponding solvent.
- (5) How is the intrinsic viscosity changing in case that the solubility of a monodisperse polymer is improved.
- (6) Which parameters are defining phase separation in binary mixtures. What are the differences between polymer solutions and polymer blends?

Recommended Books



Macromolecules
Volume 3: Physical Structures and Properties
Hans-Georg Elias

Wiley-VCH GmbH & Co. KGaA, Weihnheim 2008

Polymer Solutions
An introduction to physical properties
Iwao Teraoka

Wiley-Interscience 2002



Macromolecules

Volume 3: Physical Structures and Properties

